WHAT	IS	CL	_AI	MI	ED	<u> IS</u> :

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2 3 1. A process for oligomerizing a Fischer-Tropsch derived feed containing 4 oxygenates which comprises: 5 reducing significantly the oxygenates present in the (a) 6 Fischer-Tropsch derived feed by contacting said feed with a 7 8 hydrotreating catalyst under hydrotreating conditions in a hydrotreating zone and recovering from the hydrotreating zone a 9 Fischer-Tropsch derived hydrotreated feed which contains a 10 significantly reduced amount of oxygenates as compared to the 11 Fischer-Tropsch derived feed and also a significant amount of 12 13 paraffins; 14 15 (b) pyrolyzing the Fischer-Tropsch derived hydrotreated feed in a 16 thermal cracking zone under thermal cracking conditions 17 pre-selected to crack the paraffin molecules to form olefins and 18 collecting an olefin-enriched Fischer-Tropsch feed from the 19 thermal cracking zone; 20 21 (c) contacting the olefin-enriched Fischer-Tropsch feed with a Lewis 22 acid ionic liquid catalyst in an oligomerization zone under oligomerization reaction conditions; and 23 24 25 (d) recovering from the oligomerization zone a Fischer-Tropsch 26 derived product having molecules characterized by a higher 27 average molecular weight and increased branching as 28 compared to the Fischer-Tropsch derived feed.

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2. The process of claim 1 wherein the Fischer-Tropsch derived hydrotreated feed is substantially free of oxygenates.

2		hydrotreated feed contains less than 200 ppmw elemental oxygen.
3 4	4.	The process of claim 3 wherein the Fischer-Tropsch derived
	4.	·
5		hydrotreated feed contains less than 100 ppmw elemental oxygen.
6	_	
7	5.	The process of claim 1 wherein the hydrotreating catalyst is a
8		non-acidic hydrotreating catalyst.
9		
10	6.	The process of claim 5 wherein the hydrotreating catalyst contains the
11		metal nickel and molybdenum.
12		
13	7.	The process of claim 1 wherein the hydrotreating conditions in the
14		hydrotreating zone include a temperature of between about
15		400 degrees F and about 800 degrees F, an LHSV of between about
16		0.5 and about 5.0, and a total pressure between about 200 psig and
17		about 2,000 psig.
18		
19	8.	The process of claim 7 wherein the temperature in the hydrotreating
20		zone is less than about 675 degrees F.
21		
22	9.	The process of claim 7 wherein the LHSV is between about 1 and
23		about 4.0.
24		
25	10.	The process of claim 1 wherein the temperature in the thermal cracking
26		zone is within the range of from about 950 degrees F and about
27		1,600 degrees F.
28		
29	11.	The process of claim 1 wherein the pressure in the thermal cracking
30		zone is within the range of from about to about 0 atmospheres and
31		about 5 atmospheres.

The process of claim 2 wherein the Fischer-Tropsch derived

1 3.

1 12. The process of claim 11 wherein the pressure in the thermal cracking 2 zone is within the range of from about to about 0 atmospheres and 3 about 2 atmospheres. 4 The process of claim 1 wherein the cracking conversion in the thermal 13. 5 6 cracking zone is greater than about 10 weight percent of the paraffins 7 present. 8 The process of claim 1 wherein the ionic liquid oligomerization catalyst 9 14. comprises a first component and a second component, said first 10 11 component comprising a compound selected from the group consisting of aluminum halide, alkyl aluminum halide, gallium halide, and alkyl 12 13 gallium halide, and said second component is a quaternary ammonium, 14 or quaternary phosphonium salt. 15 The process of claim 14 wherein the ratio of the first component to the 16 15. second component is within the range of from about 1:1 to about 2:1. 17 18 19 16. The process of claim 14 wherein said first component is aluminum 20 halide or alkyl aluminum halide. 21 22 17.[^] The process of claim 14 wherein said second component is selected 23 from one or more of hydrocarbyl substituted ammonium halide, hydrocarbyl substituted imidazolium halide, hydrocarbyl substituted 24 25 pyridinium halide, alkylene substituted pyridinium dihalide, or 26 hydrocarbyl substituted phosphonium halide. 27 The process of claim 1 including the additional step of dewaxing the 28 18. Fischer-Tropsch derived product recovered from the oligomerization 29 30 zone and collecting a dewaxed Fischer-Tropsch product having 31 improved cold flow properties relative to the Fischer-Tropsch derived

product recovered from the oligomerization zone.

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1	19.		to the development the Pischer-Tropson derived product
2		is ca	talytically dewaxed.
3 4	20.	The	process of claim 18 including the additional step of hydrofinishing
5		the d	lewaxed Fischer-Tropsch product.
6			
7	21.	The	process of claim 1 wherein the Fischer-Tropsch derived product
8		inclu	des lubricant base oil.
9			
10	22.	The	process of claim 1 wherein the Fischer-Tropsch derived product
11		inclu	des a diesel product.
12			
13	23.	A pro	ocess for producing Fischer-Tropsch derived lubricant base oil
14		whic	h comprises:
15			
16		(a)	recovering from a Fischer-Tropsch plant a wax fraction;
17			····
18		(b)	reducing significantly the oxygenates present in the
19			Fischer-Tropsch wax fraction by contacting said wax fraction
20			with a hydrotreating catalyst under hydrotreating conditions in a
21			hydrotreating zone and recovering from the hydrotreating zone a
22			hydrotreated Fischer-Tropsch derived wax feed which contains
23			a significantly reduced amount of oxygenates as compared to
24			the Fischer-Tropsch derived wax fraction and also a significant
25			amount of paraffins;
26			
27		(c)	pyrolyzing the hydrotreated Fischer-Tropsch derived wax feed in
28			a thermal cracking zone under thermal cracking conditions
29			pre-selected to crack the paraffin molecules to form olefins and
30			collecting an olefin-enriched Fischer-Tropsch feed from the
21			thormal cracking zono:

1		(d)	contacting the olefin-enriched Fischer-Tropsch feed with a Lewis
2			acid ionic liquid catalyst in an oligomerization zone under
3			oligomerization reaction conditions;
4			
5		(e)	recovering from the oligomerization zone a Fischer-Tropsch
6			derived oligomerization effluent having molecules characterized
7			by a higher average molecular weight and increased branching
8			as compared to the Fischer-Tropsch derived feed;
9			
10		(f)	catalytically dewaxing the Fischer-Tropsch derived
11			oligomerization effluent by contacting the Fischer-Tropsch
12			derived oligomerization effluent with a dewaxing catalyst under
13			catalytic conditions in a dewaxing zone and collecting a
14			dewaxed Fischer-Tropsch product from the dewaxing zone
15			having improved cold flow properties relative to the
16			Fischer-Tropsch derived oligomerization effluent;
17			
18		(g)	hydrofinishing the dewaxed Fischer-Tropsch product in a
19			hydrofinishing zone under hydrofinishing conditions in the
20			presence of a hydrofinishing catalyst; and
21			
22	•	(h)	collecting a Fischer-Tropsch derived lubricant base oil from the
23			hydrofinishing zone.
24			
25	24.	The	process of claim 23 wherein the oxygenates in the hydrotreated
26			her-Tropsch derived wax feed recovered from the hydrotreating
27			e is substantially oxygenate free.
28	25.	The	process of claim 24 wherein the hydrotreated Fischer-Tropsch
29		deriv	ved wax feed recovered from the hydrotreating zone contains less
30		than	200 ppmw elemental oxygen.

1	26.	A pro	ocess for producing Fischer-Tropsch derived lubricant base oil		
2		whic	vhich comprises:		
3					
4		(a)	recovering from a Fischer-Tropsch plant a condensate fraction;		
5					
6		(b)	removing substantially all of the oxygenates present in the		
7			Fischer-Tropsch condensate fraction by contacting said		
8			condensate fraction with a hydrotreating catalyst under		
9			hydrotreating conditions in a hydrotreating zone and recovering		
10	1		from the hydrotreating zone a substantially oxygenate-free		
11			Fischer-Tropsch derived condensate feed which also contains a		
12			significant amount of paraffins;		
13					
14		(c)	pyrolyzing the substantially oxygenate-free Fischer-Tropsch		
15			derived condensate feed in a thermal cracking zone under		
16			thermal cracking conditions pre-selected to crack the paraffin		
17			molecules to form olefins and collecting an olefin-enriched		
18			Fischer-Tropsch feed from the thermal cracking zone;		
19					
20		(d)	contacting the olefin-enriched Fischer-Tropsch feed with a Lewis		
21		1	acid ionic liquid catalyst in an oligomerization zone under		
22			oligomerization reaction conditions;		
23					
24		(e)	recovering from the oligomerization zone a Fischer-Tropsch		
25			derived oligomerization effluent having molecules characterized		
26			by a higher average molecular weight and increased branching		
27			as compared to the Fischer-Tropsch derived feed;		
28		(f)	catalytically dewaxing the Fischer-Tropsch derived		
29			oligomerization effluent by contacting the Fischer-Tropsch		
30			derived oligomerization effluent with a dewaxing catalyst under		
31			catalytic conditions in a dewaxing zone and collecting a		
32			dewayed Fischer-Tropsch product from the dewaying zone		

1		having improved cold flow properties relative to the
2		Fischer-Tropsch derived oligomerization effluent;
3		
4		(g) hydrofinishing the dewaxed Fischer-Tropsch product in a
5		hydrofinishing zone under hydrofinshing conditions in the
6		presence of a hydrofinishing catalyst; and
7		
8		(h) collecting a Fischer-Tropsch derived lubricant base oil from the
9		hydrofinishing zone.
10		
11	27.	The process of claim 26 wherein the substantially oxygenate-free
12		Fischer-Tropsch derived condensate feed recovered from the
13		hydrotreating zone contains less than 200 ppmw elemental oxygen.
14		
15	28.	The process of claim 27 wherein the substantially oxygenate-free
16		Fischer-Tropsch derived condensate feed recovered from the
17		hydrotreating zone contains less than 100 ppmw elemental oxygen.
18		
19	29.	The process of claim 26 wherein a diesel product is also collected from
20		the hydrofinishing zone.